

NOAA Technical Memorandum NWS WR-122



A METHOD FOR TRANSFORMING TEMPERATURE DISTRIBUTIONS TO NORMALITY

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Salt Lake City, Utah
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NATIONAL OCEANIC AND
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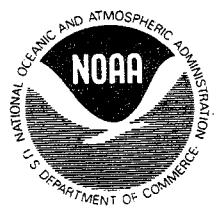
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LIST OF SYMBOLS

Symbols Used In Text	Equivalent Symbols Used In Appendix	
A	A	A term equal to $\ln(\bar{T}') - \frac{\sum \ln(T_i')}{N}$.
\hat{a}	\hat{a}	A term in the gamma distribution equal to $\frac{1 + \sqrt{1 + (4/3)A}}{4A}$.
\hat{B}	\hat{B}	A term in the gamma distribution equal to $\frac{T'}{\hat{a}}$.
N	N	Number of elements in the distribution.
P(T)	P(x)	The cumulative frequency of T.
Q(T)	Q(x)	A term equal to $1 - P(T)$.
S	S	Standard deviation.
T	x	Temperature.
\bar{T}	\bar{x}	Mean temperature.
T'	x'	The absolute value of $T - T_{\text{BASE}}$.
T_{BASE}	x_{BASE}	Base temperature.
T_i	x_i	A sample temperature of the distribution where $i = 1, 2, \dots, N$.
T_i'	x_i'	The absolute value of $T_i - T_{\text{BASE}}$.
\bar{T}'	\bar{x}'	The mean of the T' distribution.
T_M	x_{MEDIAN}	Median temperature.
T_{MODE}	--	Mode.
T_X	$x_{\text{MAX/MIN}}$	The distribution's highest or lowest temperature, depending on the sign of the skew.
$Z_N/(N+1)$	$Z_{N/(N+1)}$	A point where the area under the standard normal curve from $-\infty$ to z is $\frac{N}{N+1} \cdot 100$ percent of the curve's total area.
3.891	$Z_{0.99995}$	The value of $Z_{0.99995}$.
$\Gamma(\hat{a})$	$\Gamma(\hat{a})$	The gamma function of a.
$\gamma(\hat{a}, T'/\hat{B})$	$\gamma(\hat{a}, x'/\hat{B})$	The incomplete gamma function of $(\hat{a}, T'/\hat{B})$.

A METHOD FOR TRANSFORMING TEMPERATURE DISTRIBUTIONS TO NORMALITY

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ABSTRACT. A method of transforming and fitting temperature distributions to the normal curve using the gamma distribution is presented. At the same time, the worth of the programmable calculator is once again demonstrated. The concept of "base temperature" is introduced in the presentation: a concept which permits the gamma distribution to be used with non-positive as well as positive values. An actual temperature distribution is transformed to normality using steps contained in a program designed to normalize meteorological variates. The resultant normal curve is then used to determine cumulative temperature probabilities.

A METHOD FOR TRANSFORMING TEMPERATURE DISTRIBUTIONS TO NORMALITY

Most meteorological variates are not normally distributed. This is true in the case of temperature, whose distributions are often skewed.

It is desirable to transform and fit skewed distributions, such as temperature, to the normal curve. This is because many useful statistical tests such as analysis of variance, hypothesis testing about the mean, etc., are valid only for normal distributions. In addition, the temperature distribution once transformed can be represented as a smooth curve on probability graph paper, thus allowing easy determination of temperature frequency.

How can temperature distributions be transformed to normality? One way is to use the gamma distribution to fit and transform the temperature distribution (Panofsky and Brier 1958). Unfortunately, the transforming process is usually tedious, involves complicated equations, and hard-to-read tables.

Enter the programmable calculator! These electronic marvels make the process of "normalizing" temperatures virtually painless, especially if the calculator is designed to accept magnetic program cards.

However, the gamma distribution can be used only if the distribution to be transformed consists of positive numbers. Obviously, temperatures expressed in ($^{\circ}$ F) or ($^{\circ}$ C) can assume values of zero or below.

One way of solving this problem is to select a "base temperature" which, when added to each temperature in the distribution, will make all the temperatures positive. The base temperature should be a few degrees lower than the distribution's lowest temperature if the distribution has positive skew, or a few degrees higher than the distribution's highest temperature if the distribution has negative skew 1/.

The author's formula for objectively determining the base temperature is as follows:

$$T_{\text{BASE}} = \sqrt{\frac{3.891}{Z \left[\frac{N}{N+1} \right]}} \cdot (T_X - T_M) + T_M$$

Values of $Z \left[\frac{N}{N+1} \right]$ can be obtained from Figure 1.

The program to normalize meteorological distributions consists of 435 steps 2/. It is designed to run on a Texas Instruments SR-52 calculator. The program flowchart is shown in Figure 2.

For purposes of illustration, the author will show how January minimum temperatures at Laramie, Wyoming, are transformed to normality using steps outlined in the program 3/. Laramie's winter temperature distributions show large skew and wide extremes--in other words, a good test for the program.

The sample temperatures are selected and the resultant distribution checked for the sign of its skew. In this case, a random sample of 100 elements is selected from a population of 620 January minimum temperatures at Laramie. The sample temperatures are then arrayed, as in Table 1. Since $T_M = 12^{\circ}\text{F}$, $T_{\text{MODE}} = 14^{\circ}\text{F}$, and $T_X = 33^{\circ}\text{F}$ (maximum T_i) and -46°F (minimum T_i), the sample distribution is assumed to have negative skew.

T_{BASE} needs to be determined, because the distribution has negative skew and contains temperatures $\leq 0^{\circ}\text{F}$. Since $N = 100$, $N/(N+1) = 100/101 = 0.9900990099$. Using Figure 1, $Z_{100/101}$ is found to be equal to

1/ $\sum |T_i - T_{\text{BASE}}|$ should be kept as small as possible. Otherwise $\Gamma(\alpha)$, a term influenced by the size of $\sum |T_i - T_{\text{BASE}}|$, will become too large for the calculator to handle.

2/ See appendix.

3/ The author had previously normalized Laramie's temperatures, while stationed at WSFO Cheyenne.

2.33. Substituting 12°F for T_M , 33°F for T_X , and 2.33 for $Z_N/(N+1)$ yields a T_{BASE} of $39.13763204^{\circ}\text{F}$. Pressing the keys FIX, 0, and RUN truncates the fractional part of the number and places the integer 39 in the data register reserved for T_{BASE} .

The next steps involve the computation of sums which are used to solve later equations. Each T_i is entered into the program by successive keystrokes, with sums for T_i , T_i^2 , $T_i' = |T_i - T_{\text{BASE}}|$, $\ln(T_i')$, and i accumulated in appropriate data registers. After all 100 temperatures are entered, the following sums are obtained:

$$\sum T_i = 997$$

$$\sum T_i^2 = 28,953$$

$$\sum T_i' = 2,903$$

$$\sum \ln(T_i') = 325.5576843\cdots$$

The above sums are used to solve equations for the distribution's mean, standard deviation and skew, and the terms A, \hat{a} , and \hat{b} which are used to compute $\Gamma(\hat{a})$ and values of $\gamma(\hat{a}, T'/\hat{b})$. Substituting the appropriate data register contents into the equations yield the following:

$$\bar{T} = \sum T_i/N = 997/100 = \underline{9.97^{\circ}\text{F}}$$

$$S = \sqrt{(\sum T_i^2 - NT^2)/(N - 1)} = \sqrt{(28,953 - 100(9.97)^2)/(100 - 1)} \\ = \underline{13.86^{\circ}\text{F}}$$

$$\text{SKEN} = 3(\bar{T} - T_M)/S = 3(9.97 - 12)/13.86 = \underline{-0.439}$$

$$A = \ln(\sum T_i'/N) - \sum \ln(T_i')/N = \ln(2,903/100) - 325.5576843\cdots/100 \\ = \underline{0.1127529346\cdots}$$

$$\hat{a} = (1 + \sqrt{1 + (4/3)A})/4A = \frac{(1 + \sqrt{1 + (4/3) \cdot (0.1127529346\cdots)})}{4(0.1127529346\cdots)} \\ = \underline{4.595307802\cdots}$$

$$\hat{b} = (\sum T_i'^2/N)/\hat{a} = (2,903/100)/4.595307802\cdots = \underline{6.317313496\cdots}$$

$$\Gamma(\hat{a}) = \int_0^{\hat{a}} t^{\hat{a}-1} e^{-t} dt$$

$$\approx \frac{\sqrt{2\pi} \cdot (\hat{a}+5)^{(\hat{a}+5)} e^{-[(\hat{a}+5)]}}{(\hat{a}+4) \cdot (\hat{a}+3) \cdot (\hat{a}+2) \cdot (\hat{a}+1) \cdot \hat{a}} \left[\frac{1}{12(\hat{a}+5)} + \frac{1}{360(\hat{a}+5)^3} \right]$$

$$= \underline{13.29286832\cdots}, \text{ with error}/\Gamma(\hat{a}) < 2(10^{-7})$$

$$\text{Thus, error} < \underline{2.7(10^{-6})}$$

4/ The two dots preceding the superscript indicate the number is accurate to 12 significant digits in the data register. However, the display register in the SR-52 is capable of showing only 10 of these digits.

The solutions for \hat{a} , \hat{B} , and $\Gamma(\hat{a})$ are stored in data registers, so they can be recalled for subsequent computations.

By entering a temperature T into the program at this point, a value of the incomplete gamma function corresponding to T' can be obtained. The formula for the incomplete gamma function is:

$$\gamma(\hat{a}, T'/\hat{B}) = \int_0^{T'/\hat{B}} t^{\hat{a}-1} e^{-t} dt$$
$$= (T'/\hat{B})^{\hat{a}} \cdot e^{-(T'/\hat{B})} \sum_{n=0}^{\infty} \frac{(T'/\hat{B})^n}{\hat{a}(\hat{a}+1) \cdots (\hat{a}+n)}.$$

An iterative technique is used to solve the above formula. The iterative process continues until the series portion of the formula achieves a predetermined accuracy--in this case, accuracy to seven significant figures. The series is then multiplied by the terms preceding it, yielding a value of the incomplete gamma function.

Dividing $\gamma(\hat{a}, T'/\hat{B})$ by $\Gamma(\hat{a})$ yields the cumulative frequencies $P(T)$ and $Q(T) = [1 - P(T)]$ for a temperature T . Values of $\gamma(\hat{a}, T'/\hat{B})$, $P(T)$, and $Q(T)$ for selected January minimum temperatures at Laramie are listed in Table 2.

Information concerning temperature which was previously unknown or hard to determine can be easily interpolated from fitted gamma distributions such as the one in Figure 3. The January minimum temperature at Laramie should be $>28^{\circ}\text{F}$ in only about 5 percent of the observations; 21 percent of the observed minimums should be $<0^{\circ}\text{F}$; 80 percent of the observations should lie between -8°F and 25°F , with 36 percent of the observations being between 16°F and 32°F . In other words, the gamma curve makes it easy to express temperature data in probabilistic terms.

Thus, temperatures as well as other meteorological distributions can be transformed to normality by using the gamma distribution as a transforming agent. The process can be hastened considerably and actually made easy by letting a programmable calculator do the dirty work. Hopefully, this presentation will prove useful to those who wish to try the method out at their own station, or on other meteorological variates.

ACKNOWLEDGEMENTS. The author wishes to express his sincere thanks to Robert G. Beebe, Meteorologist in Charge of WSFO, Cheyenne, Wyoming. Bob's leadership, which encouraged on-station research while the author was stationed at Cheyenne, was the main inspiration for this paper. I also wish to thank my wife, Mary, who faithfully served as a proofreader and favorite critic as the paper evolved.

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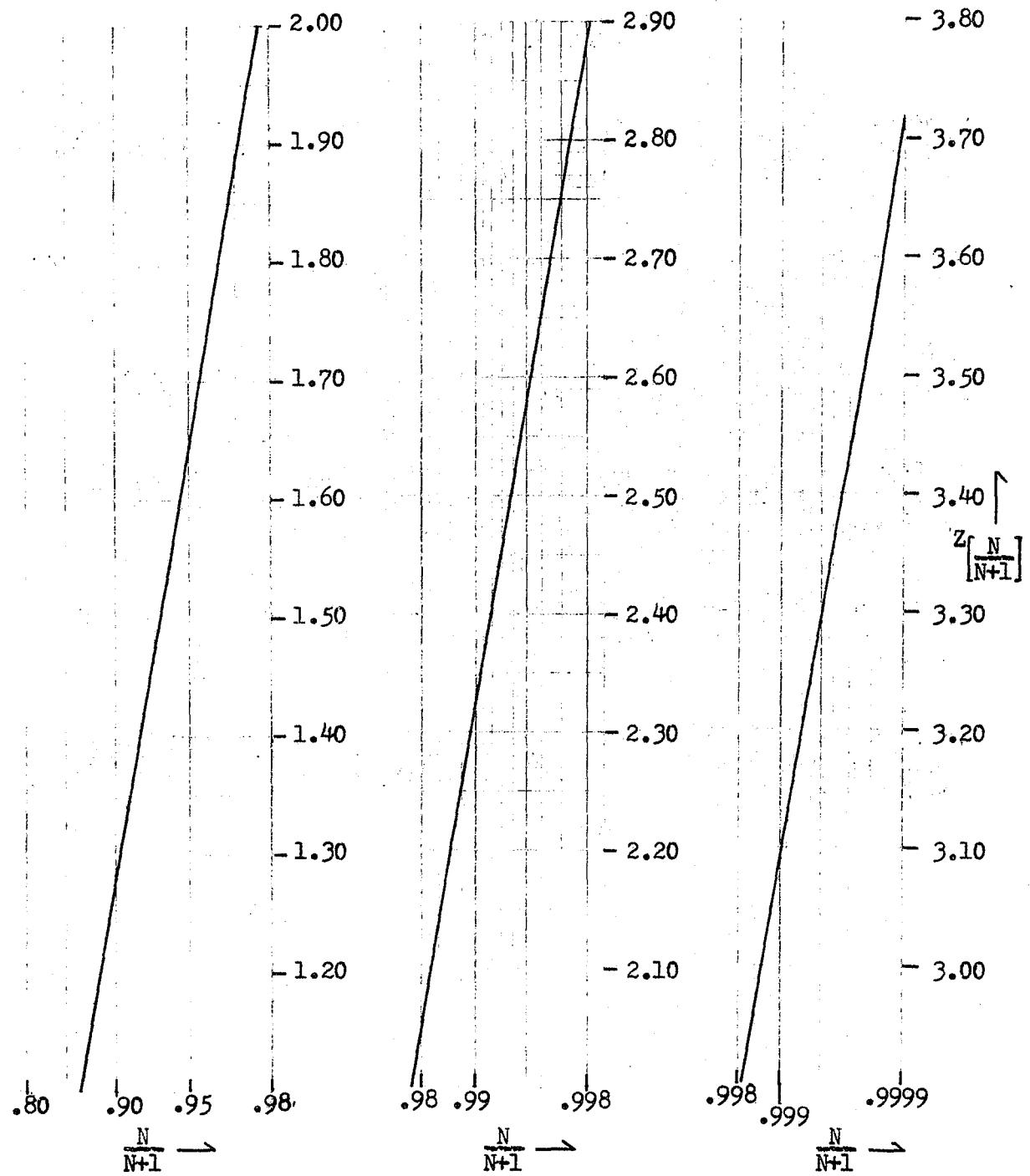


Figure 1. Graph Depicting $N/(N+1)$ vs. $Z_{N/(N+1)}$.

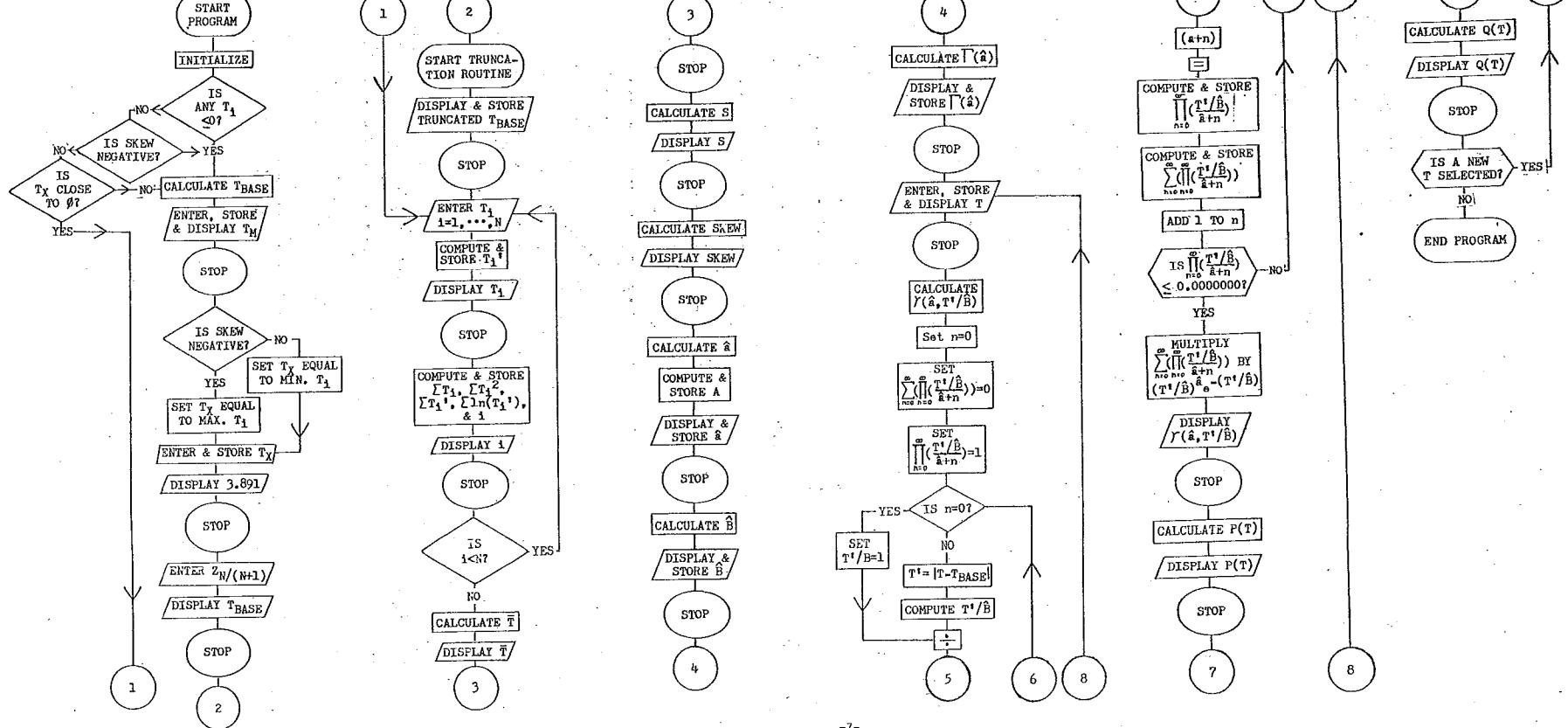


Figure 2. Flowchart of the Program Which Transforms Temperature Distributions to Normality

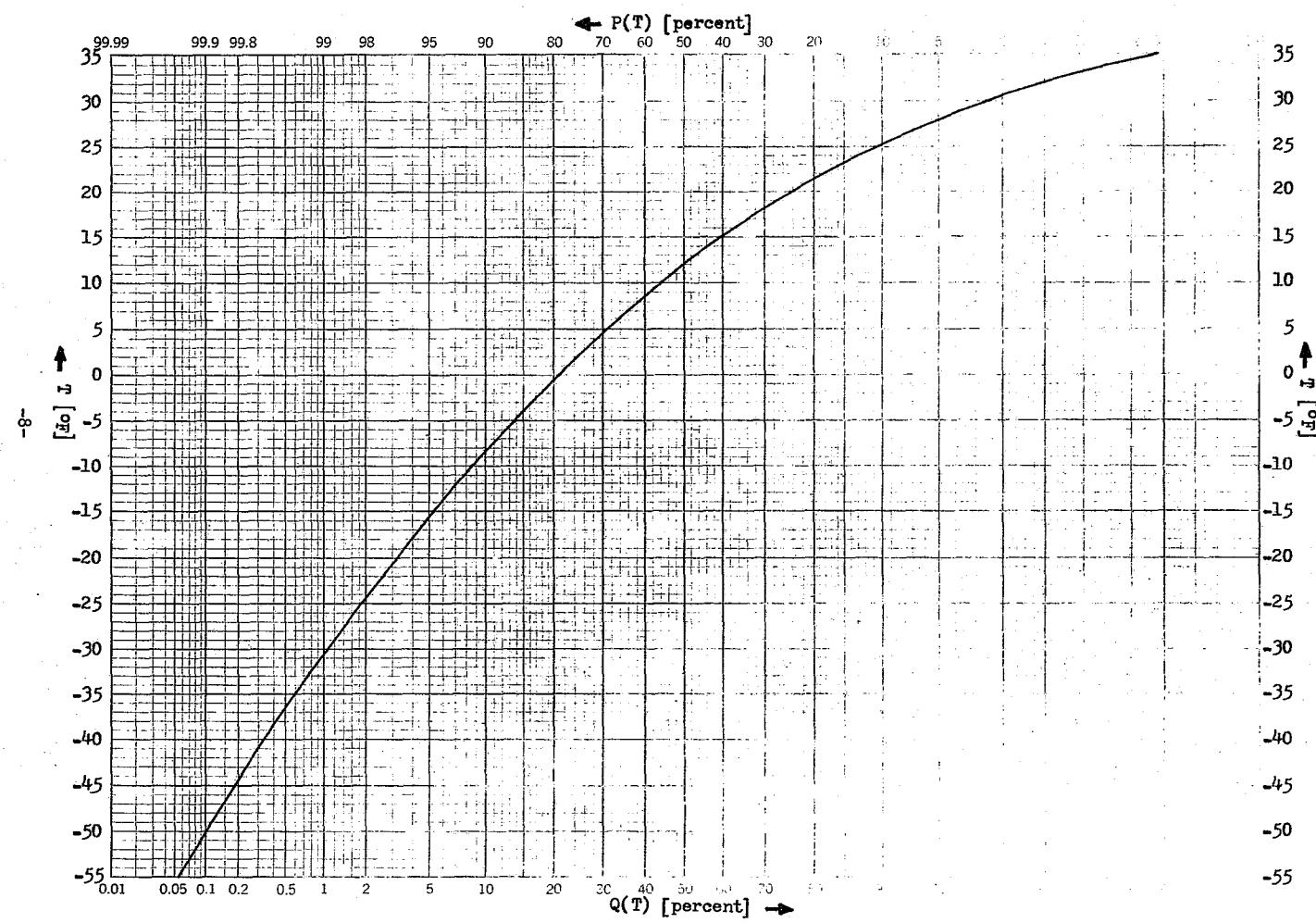


Figure 3. Graph Depicting the January Minimum Temperature at Laramie, Wyoming, (T) vs. the Cumulative Frequency of Temperature [$P(T)$ and $Q(T)$].

TABLE 1

SAMPLE OF 100 JANUARY MINIMUM TEMPERATURES AT LARAMIE, WYOMING
USED TO TEST THE PROGRAM
(TEMPERATURES ARRANGED FROM HIGHEST TO LOWEST VALUE)

i	T _i (°F)	i	T _i (°F)	i	T _i (°F)
1	33	41	14	81	1
2	33	42	14	82	0
3	31	43	14	83	0
4	30	44	14	84	0
5	29	45	14	85	-1
6	27	46	14	86	-1
7	27	47	14	87	-2
8	26	48	13	88	-4
9	25	49	13	89	-5
10	25	50	12	90	-7
11	25	51	12	91	-8
12	24	52	11	92	-13
13	24	53	11	93	-13
14	23	54	10	94	-15
15	23	55	10	95	-16
16	23	56	10	96	-17
17	22	57	10	97	-18
18	22	58	9	98	-22
19	22	59	9	99	-33
20	22	60	9	100	-46
21	21	61	9		
22	21	62	8		
23	20	63	8		
24	20	64	8		
25	20	65	7		
26	19	66	7		
27	19	67	6		
28	18	68	6		
29	18	69	5		
30	18	70	5		
31	18	71	5		
32	18	72	5		
33	17	73	5		
34	17	74	4		
35	17	75	3		
36	17	76	3		
37	17	77	2		
38	16	78	2		
39	16	79	2		
40	15	80	2		

TABLE 2

VALUES OF $\gamma(a, T^*/B)$, P(T), AND Q(T) FOR SELECTED
JANUARY MINIMUM TEMPERATURES AT LARAMIE, WYOMING

T(°F)	$\gamma(\hat{a}, T^*/\hat{B})$	P(T)	Q(T)
37	0.00085	0.00006	0.99994
35	0.01592	0.00120	0.99880
30	0.35198	0.02648	0.97352
25	1.45297	0.10930	0.89070
20	3.26784	0.24583	0.75417
15	5.40220	0.40640	0.59360
12	6.66542	0.50143	0.49857
10	7.46000	0.56120	0.43880
5	9.20132	0.69220	0.30780
0	10.54511	0.79329	0.20671
-5	11.51347	0.86614	0.13386
-10	12.17533	0.91593	0.08407
-15	12.60905	0.94856	0.05144
-20	12.88370	0.96922	0.03078
-25	13.05274	0.98194	0.01806
-30	13.15430	0.98958	0.01042
-35	13.21409	0.99407	0.00593
-40	13.24867	0.99668	0.00332
-45	13.26836	0.99816	0.00184
-50	13.27942	0.99899	0.00101
-55	13.28556	0.99956	0.00055
-60	13.28893	0.99970	0.00030

APPENDIX

ACTUAL SR-52 PROGRAM
USED TO NORMALIZE METEOROLOGICAL VARIATES

(X replaces T in most of the symbology, since the program is used to normalize meteorological variates other than temperature).

SR-52
User Instructions

MEAN, STANDARD DEVIATION,
SKEW, \hat{A} , AND \hat{B}

PAGE 1 OF 3

A				
X _{BASE}	\bar{x}	s	skew	INIT.
x _i	i	a	b	MEDIAN

B				

STEP	PROCEDURE	ENTER	PRESS	DISPLAY
1	LOAD PROGRAM CARD			
2	CLEAR REGISTERS		*E'	Ø
3	ENTER MEDIAN	X MEDIAN	E	X MEDIAN
4	CALCULATE X _{BASE}	X MAX/MIN	*A'	3.891
	= $\sqrt{\frac{2}{N(N+1)} \cdot [X_{MAX/MIN} - X_{MEDIAN}]}$	$\bar{x} [N/(N+1)]$	RUN	X _{BASE}
	+ X MEDIAN	*FIX M, M=0,..,9	RUN	X _{BASE} (TRUNCATED TO M DECIMAL PLACES)
	NOTE: USE STEPS 3 AND 4 WHEN ANY OF THE X _i 'S ARE ≤ 0 , AND/OR WHEN THE DISTRIBUTION HAS A NEGATIVE SKEW.			
5	INDEPENDENT VARIABLE X _i	X _i	A	X _i
			B	i, i=1,..,N
	REPEAT STEP 5 FOR ALL X _i 'S IN THE DISTRIBUTION			
6	COMPUTE THE MEAN		*B'	\bar{x}
7	COMPUTE THE STANDARD DEVIATION		*C'	S
8	COMPUTE THE SKEW		*D'	SKW
9	COMPUTE \hat{A}		C	\hat{A}
10	COMPUTE \hat{B}		D	\hat{B}
	$\bar{x} = \sum_{i=1}^N x_i / N$			
	$S = \sqrt{\frac{1}{N-1} \left(\sum_{i=1}^N x_i^2 - N \bar{x}^2 \right)}$			
	SKEW = $\frac{3(\bar{x} - X_{MEDIAN})}{S}$			
	$\hat{A} = [1 + \sqrt{1 + 4A/3}] / 4A$ WHERE $A = \ln \bar{x}' - \frac{1}{N} \sum_{i=1}^N \ln x'_i$, $x'_i = x_i - X_{BASE} $			
	$\hat{B} = \bar{x}' / \hat{A}$ WHERE $\bar{x}' = [\sum_{i=1}^N x_i - X_{BASE}] / N$			

TITLE \bar{x} , S, SKEW, \hat{A} , AND \hat{B}
PROGRAMMER MORRIS S. WEBB, JR. PAGE 2 OF 3
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Coding Form

LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LABELS
000	46	*LBL			54)			ØØ	Ø	$\sum x_i$	A X;
	17	*B'			56	*RTN			ØØ	8	$\sum_{i=1}^n ln x_i$	B i
	53	(040	46	*LBL			23	LNX		C \hat{A}
	43	RCL			11	A			44	SUM	\sum_n	D \hat{B}
	ØØ	Ø	COMPUTE		53	(080	ØØ	Ø	$\sum_{i=1}^n ln x_i$	E X MEDIAN
005	Ø6	6	\bar{x}		42	STO			Ø9	9	$\sum_{i=1}^n ln x_i$	A' X BASE
	55	-			ØØ	Ø			Ø1	1		B' \bar{x}
	43	RCL		045	Ø4	4			44	SUM		C' S
	Ø1	1			75	-			Ø1	1	N	D' SKEW
	ØØ	Ø			43	RCL	COMPUTE	085	ØØ	Ø		E' INIT.
010	54)			ØØ	Ø	X_i		43	RCL		REGISTERS
	56	*RTN			Ø3	3	$= x_i - X_{BASE} $		Ø1	1	DISPLAY	00
	46	*LBL		050	54)	AND DIS-		ØØ	Ø	N	D1 MEDIAN
	18	*C'			4Ø	*X ²	PLAY X _i		81	HLT		D2 X MAX/MIN
	53	(3Ø	* $\sqrt{ }$		090	46	*LBL		D3 X BASE
015	53	(42	STO			13	C	COMPUTE	D4 X i
	53	(ØØ	Ø			53	(\hat{A}	D5 X i
	43	RCL		055	Ø5	5			53	(AND STORE	D6 $\sum X$
	ØØ	Ø			43	RCL			43	RCL	IN R ₁₂	D7 $\sum X^2$
	Ø7	7			ØØ	Ø		095	ØØ	Ø		D8 $\sum X'$
020	75	-			Ø4	4			Ø8	8		D9 $\sum ln x'$
	43	RCL			81	HLT			55	-		D10 N
	Ø1	1			060	46	*LBL	096	43	RCL		D11 A
	ØØ	Ø			12	B	SUMS		Ø1	1		D12 \hat{A}
	65	X			43	RCL		100	ØØ	Ø		D13 \hat{B}
025	17	*B'	COMPUTE		ØØ	Ø			54)	(COMPUTE	D14
	4Ø	*X ²	S		Ø4	4			23	LNX	A AND	D15
	54)		065	44	SUM	$\sum x_i$		75	-	STORE	D16
	55	-			ØØ	Ø	$\sum_{i=1}^n x_i$		43	RCL	IN R ₁₁	D17
	53	(Ø6	6		105	ØØ	Ø		D18
030	43	RCL			4Ø	*X ²			Ø9	9		D19
	Ø1	1			44	SUM	$\sum x_i^2$		55	-		FLAGS
	ØØ	Ø		070	ØØ	Ø	$\sum x_i^2$		43	RCL		0
	75	-			Ø7	7	$\sum_{i=1}^n x_i^2$		Ø1	1		1
	Ø1	1			43	RCL		110	ØØ	Ø		2
035	54)			ØØ	Ø			54)		3
	54)			Ø5	5						4
	3Ø	* $\sqrt{ }$		075	44	SUM						

TITLE X, S, SKEW: $\hat{\alpha}$ AND $\hat{\beta}$
 PROGRAMMER MORRIS S. WEBB, JR.
 DATE 4/16/77

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 Coding Form

LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LABELS
112	42	STO		150	00	Ø	R ₁₃	192	43	RCL		A X _i
	Ø1	*	1		55	:				Ø0	Ø	B i
	Ø1	1		152	43	RCL			Ø1	1	C $\hat{\alpha}$	
	53	(Ø1	1			95	=	D $\hat{\beta}$	
	53	(Ø2	2		192	81	HLT	(INSERT FIXM M=0,...,9)	E X _{MEDIAN}
117	Ø4	4			95	=			52	EE	A' X _{BASE}	
	55	÷		157	42	STO			22	INV	B' X	
	Ø3	3			Ø1	1			52	EE	C' S	
	65	X			Ø3	3			22	INV	D' SKEW	
	43	RCL			81	HLT		197	57	*FIX	E' INIT.	
122	Ø1	1	COMPUTE		46	*LBL			42	STO	DISPLAY	
	Ø1	1	$\hat{\alpha}$		15	E	STORE		Ø0	Ø	REGISTERS	
	85	+	AND STORE	162	42	STO	MEDIAN		Ø3	3	00	
	Ø1	1	IN R ₁₂		ØØ	Ø	IN		81	HLT	01 MEDIAN	
	54)			Ø1	1	R ₀₁	202	46	*LBL	02 X _{MAX/UN}	
127	30	*√			81	HLT			19	*D'	03 X _{BASE}	
	85	+			46	*LBL			53	(04 X _i	
	Ø1	1		167	16	*A'	COMPUTE		17	*B'	05 X ₁	
	54)			42	STO	X _{BASE}		75	-	06 ΣX	
	55	÷			Ø0	Ø		207	43	RCL	07 ΣX^2	
132	Ø4	4			Ø2	2			ØØ	Ø	08 $\Sigma X'$	
	55	÷			75	-			09 $\Sigma \ln X^*$	09 $\Sigma \ln X^*$		
	43	RCL		172	43	RCL			Ø1	1	10 N	
	Ø1	1			Ø0	Ø			54)	11 A	
	Ø1	1			Ø1	1			65	X	12 $\hat{\alpha}$	
137	95	=			95	=			212	Ø3	13 $\hat{\beta}$	
	42	STO			65	X			55	÷	14	
	Ø1	1		177	53	(18	*C'	15	
	Ø2	2			Ø3	3			95	=	16	
	81	HLT			81	HLT			217	46	17	
142	46	*LBL			93	.			10	*E'	CLEAR	
	14	D			Ø8	8	(Z _{0.99995})		47	*CMS	FLAGS	
	43	RCL		182	Ø1	1			25	CLR	0	
	ØØ	Ø			55	÷			81	HLT	1	
	Ø8	8			81	HLT	(INSERT Z[N/(N+1)])	222			2	
147	55	...	COMPUTE		54)					3	
	43	RCL	$\hat{\beta}$ AND		30	*√					4	
	Ø1	1	STORE IN	187	85	+						

GAMMA FUNCTION
 AND INCOMPLETE GAMMA FUNCTION

$\leftarrow A \rightarrow$	$(\hat{\alpha} + 5) x^{\hat{\beta}}$	$x^{\hat{\beta}}$	$\Gamma(\hat{\alpha})$	$P(x)$	$Q(x)$
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 User Instructions

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$\leftarrow B \rightarrow$	$x^{\hat{\beta}}$	$\Gamma(\hat{\alpha}, x^{\hat{\beta}})$	$P(x)$	$Q(x)$
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STEP	PROCEDURE	ENTER	PRESS	DISPLAY
	THE "MEAN, STANDARD DEVIATION, ... , B" PROGRAM IS TO BE USED PRIOR TO STEP 1.			
1	LOAD PROGRAM CARD			
2	CALCULATE $\Gamma(\hat{\alpha})$	A		$\Gamma(\hat{\alpha})$
3	INDEPENDENT VARIABLE X	X		X
4	CALCULATE $\Gamma(\hat{\alpha}, x^{\hat{\beta}})$ (UNROUNDED).	C		$\Gamma(\hat{\alpha}, x^{\hat{\beta}})$ (UNROUNDED).
5	CALCULATE P(x)	D		P(x) (TO FIVE DECIMAL PLACES).
6	CALCULATE Q(x)	E		Q(x) (TO FIVE DECIMAL PLACES).
	REPEAT STEPS. 3-6 FOR EACH X.			
	To see $(\hat{\alpha} + 5)$	*A'		
	To see $x^{\hat{\beta}}$	*B'		
	$\Gamma(\hat{\alpha}) = \int_{0}^{\infty} x^{\hat{\alpha}-1} e^{-x} dx \cong \sqrt{\frac{2\pi}{(\hat{\alpha}+5)}} \cdot (\hat{\alpha}+5)^{-(\hat{\alpha}+5)} - \frac{1}{2(\hat{\alpha}+5)} + \frac{360}{(\hat{\alpha}+5)^3}$			
	$(\hat{\alpha}+..., \hat{\alpha}+1), (\hat{\alpha}+2), (\hat{\alpha}+1), \hat{\alpha}$			
	$\Gamma(\hat{\alpha}, x^{\hat{\beta}}) = \int_{0}^{x^{\hat{\beta}}} t^{\hat{\alpha}-1} e^{-t} dt \cong (x^{\hat{\beta}})^{\hat{\alpha}-1} e^{-(x^{\hat{\beta}})} \sum_{n=0}^{\infty} \frac{(x^{\hat{\beta}})^n}{\hat{\alpha}(\hat{\alpha}+1)\dots(\hat{\alpha}+n)}$			
	$P(x) = \frac{\Gamma(\hat{\alpha}, x^{\hat{\beta}})}{\Gamma(\hat{\alpha})}$			
	$Q(x) = 1 - P(x)$			

TITLE GAMMA / INCOMPLETE GAMMA FUNCTION PAGE 2 OF 3
 PROGRAMMER MORRIS S. WEBB, Jr. DATE 5/29/77

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LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LABELS
000	46	*LBL		04	4	STEP 45)		52	EE	IF NOT,	A ^r (\hat{a})	
17	*B'			05	5			22	INV	GOTO	B X	
53	(040	17	*B' (IF n ≠ 0,		90	*IFZERO	STEP 082)	C Y($\hat{a}, x/\hat{b}$)	
53	(41	GTO	CALCULATE		00	Ø		D P(x)	
43	RCL			ØØ	Ø	X/B AND		03	3		E Q(x)	
005	ØØ	Ø		04	4	GOTO STEP		03	3		A' ($\hat{a}+5$)	
Ø4	4			Ø6	6	46)		43	RCL		B' X/Y \hat{b}	
75	-	COMPUTE		045	Ø1	1		Ø1	1		C'	
43	RCL	AND		55	÷			Ø7	7		D'	
ØØ	Ø	DISPLAY		53	(085	65	X	E'	
010	Ø3	3	X/Y \hat{b}	43	RCL			17	*B'		REGISTERS	
54)			Ø1	1	X/Y \hat{b}		45	y ^x		00	
40	*X ²			050	Ø2	2	$\hat{a}+n$	43	RCL		01 MEDIAN	
30	* \sqrt{x}			85	+			Ø1	1		02 X _{MAX/MIN}	
55	÷			43	RCL			090	Ø1	2	03 X _{BASE}	
015	43	RCL		Ø1	1			65	X		04 X _{OR X_i}	
Ø1	1			Ø5	5			17	*B'		05 X _i '	
Ø3	3			055	95	=		94	+/-	06 $\sum x$		
54)			49	*PROD	$\prod_{n=0}^{n-1} R_{16}$		22	INV		07 $\sum x^2$	
56	*RTN			Ø1	1	$= R_{16}$		23	LN X		08 $\sum x^r$	
020	46	*LBL	COMPUTE	Ø6	6			95	=	09 $\ln x^r$		
13	C	Y($\hat{a}, x/\hat{b}$)		43	RCL	RECALL		22	INV		10 N	
ØØ	Ø			Ø1	1	R_{16}		57	*FIX		11 A	
42	STO	(STORE		Ø6	6			42	STO	(STORE	12 \hat{a}	
Ø1	1	ZERO IN		44	SUM	$\sum_{n=0}^{\infty} R_{16}$		100	Ø1	1	13 \hat{b}	
025	Ø5	5	R ₁₆ AND	Ø1	1	$= R_{17}$		Ø8	8	IN R ₁₆)	14 T(\hat{a})	
42	STO	R ₁₇)		Ø7	7			81	HLT		15 n	
Ø1	1			065	Ø1	1		46	*LBL		16 $\prod_{n=0}^{n-1} R_{16}$	
Ø7	7			44	SUM	(LOOP		16	*A'		17 $\sum_{n=0}^{\infty} R_{16}$	
Ø1	1			Ø1	1	COUNTER)		105	53	(COMPUTE	18 Y($\hat{a}, x/\hat{b}$)	
030	42	STO	(STORE 1	Ø5	5			43	RCL	AND	19	
Ø1	1	IN R ₁₆)		43	RCL			Ø1	1	DISPLAY	FLAGS	
Ø6	6			070	Ø1	1		Ø2	2	($\hat{a}+5$)	0	
43	RCL	(RECALL		Ø6	6			85	+		1	
Ø1	1	n)		57	*FIX	(IF R ₁₆ >		110	Ø5	5	2	
035	Ø5	5		Ø7	7	0.0000000		54)		3	
90	*IFZERO	(IF n ≠ 0,		52	EE	GO TO				4		
ØØ	Ø	GO TO	075	22	INV	STEP Ø33;						

TITLE GAMMA / INCOMPLETE GAMMA FUNCTION PAGE 3 OF 3
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LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LABELS
112	56	*RTN		75	-			54)		A ^r (\hat{a})	
14	46	*LBL		53	(55	÷		B X	
53	(152	Ø1	1		53	(C Y($\hat{a}, x/\hat{b}$)	
43	RCL			16	*A'			16	*A'		D P(x)	
005	ØØ	Ø	X/B AND	117	Ø1	1		192	75	-	E Q(x)	
Ø4	4			117	Ø8	COMPUTE		16	*A'		A' ($\hat{a}+5$)	
75	-	COMPUTE		55	÷	P(x)		54)		B' X/Y \hat{b}	
43	RCL	AND		157	2Ø	*1/x		55	-		C'	
Ø1	1			43	RCL			85	+		D'	
ØØ	Ø	DISPLAY		Ø1	1			53	(E'	
010	Ø3	3	X/Y \hat{b}	085	65	X		197	16	*A'	REGISTERS	
54)			122	Ø4	4		Ø3	3		00	
40	*X ²			54)			Ø6	6		01 MEDIAN	
30	* \sqrt{x}			57	*FIX			162	ØØ	Ø	02 X _{MAX/MIN}	
55	÷			Ø5	5			65	X		03 X _{BASE}	
015	43	RCL		56	*RTN			16	*A'		04 X _{OR X_i}	
Ø1	1			127	43	*LBL		45	y ^x		05 X _i '	
Ø1	1			15	E			Ø3	3		06 $\sum x$	
Ø3	3			Ø1	1	COMPUTE		167	54)	07 $\sum x^2$	
54)			75	-	Q(x)		2Ø	*1/x		08 $\sum x^r$	
56	*RTN			14	D			12	B		09 $\sum \ln x^r$	
020	46	*LBL	COMPUTE	95	=			207	22	INV	ENTER	
13	C	Y($\hat{a}, x/\hat{b}$)		22	INV			94	+/-		10 N	
ØØ	Ø			81	HLT			57	*FIX	AND DIS-	11 A	
42	STO	(STORE		46	*LBL			22	INV		12 \hat{a}	
Ø1	1	ZERO IN		11	A			42	STO	PLAY X	13 \hat{b}	
025	Ø5	5	R ₁₆ AND	Ø2	2			ØØ	Ø		14 T(\hat{a})	
42	STO	R ₁₇)		65	X			Ø1	1		15 n	
Ø1	1			59	*T ^r			Ø2	2		16 $\prod_{n=0}^{n-1} R_{16}$	
Ø7	7			55	÷			177	55	÷	17 $\sum_{n=0}^{\infty} R_{16}$	
Ø1	1			16	*A'	COMPUTE		95	=	18 Y($\hat{a}, x/\hat{b}$)		
030	42	STO	(STORE 1	43	RCL	AND		16	*A'		19 FLAGS	
Ø1	1	IN R ₁₆)		Ø1	1	DISPLAY		75	-		0	
Ø6	6			Ø2	2	($\hat{a}+5$)	0	16	*A'		1	
43	RCL	(RECALL		85	+		1	45	y ^x		2	
Ø1	1	n)		110	Ø5	5	2	16	*A'		3	
035	Ø5	5		54)		3	53	(4		
90	*IFZERO	(IF n ≠ 0,					4	75	-			
ØØ	Ø	GO TO	075	22	INV	STEP Ø33;		16	*A'			

NOAA Technical Memoranda NWSWR: (Continued)

- 92 Smoke Management in the Willamette Valley. Earl M. Bates, May 1974. (COM-74-11277/AS)
93 An Operational Evaluation of 500-mb Type Stratified Regression Equations. Alexander E. MacDonald, June 1974. (COM-74-11407/AS)
94 Conditional Probability of Visibility Less than One-Half Mile in Radiation Fog at Fresno, California. John D. Thomas, August 1974. (COM-74-11555/AS)
95 Climate of Flagstaff, Arizona. Paul W. Sorenson, August 1974. (COM-74-11678/AS)
96 Map Type Precipitation Probabilities for the Western Region. Glenn E. Rasch and Alexander E. MacDonald, February 1975. (COM-75-10428/AS)
97 Eastern Pacific Cut-off Low of April 21-28, 1974. William J. Alder and George R. Miller, January 1976. (PB-250-711/AS)
98 Study on a Significant Precipitation Episode in the Western United States. Ira S. Brenner, April 1975. (COM-75-10719/AS)
99 A Study of Flash Flood Susceptibility--A Basin in Southern Arizona. Gerald Williams, August 1975. (COM-75-11360/AS)
100 A Study of Flash-Flood Occurrences at a Site Versus Over a Forecast Zone. Gerald Williams, August 1975. (COM-75-11404/AS)
102 A Set of Rules for Forecasting Temperatures in Napa and Sonoma Counties. Wesley L. Tuft, October 1975. (PB-246-902/AS)
103 Application of the National Weather Service Flash-Flood Program in the Western Region. Gerald Williams, January 1976. (PB-253-053/AS)
104 Objective Aids for Forecasting Minimum Temperatures at Reno, Nevada, During the Summer Months. Christopher D. Hill, January 1976. (PB-252-866/AS)
105 Forecasting the Mono Wind. Charles P. Ruscha, Jr., February 1976. (PB-254-650)
106 Use of MOS Forecast Parameters in Temperature Forecasting. John C. Plankinton, Jr., March 1976. (PB-254-649)
107 Map Types as Aid in Using MOS PoPs in Western United States. Ira S. Brenner, August 1976. (PB259594)
108 Other Kinds of Wind Shear. Christopher D. Hill, August 1976. (PB260437/AS)
109 Forecasting North Winds in the Upper Sacramento Valley and Adjoining Forests. Christopher E. Fontana, September 1976.
110 Cool Inflow as a Weakening Influence on Eastern Pacific Tropical Cyclones. William J. Denney, November 1976. (PB 264655/AS)
111 Operational Forecasting Using Automated Guidance. Leonard W. Snellman, February 1977.
112 The MAN/MOS Program. Alexander E. MacDonald, February 1977. (PB 265941/AS)
113 Winter Season Minimum Temperature Formula for Bakersfield, California, Using Multiple Regression. Michael J. Oard, February 1977.
114 Tropical Cyclone Kathleen. James R. Fors, February 1977.
115 Program to Calculate Winds Aloft Using a Hewlett-Packard 25 Hand Calculator. Brian Finke, February 1977.
116 A Study of Wind Gusts on Lake Mead. Bradley Colman, April 1977.
117 The Relative Frequency of Cumulonimbus Clouds at the Nevada Test Site as a Function of K-value. R. F. Quiring, April 1977.
118 Moisture Distribution Modification by Upward Vertical Motion. Ira S. Brenner, April 1977.
119 Relative Frequency of Occurrence of Warm Season Echo Activity as a Function of Stability Indices Computed from the Yucca Flat, Nevada, Rawinsonde. Darryl Randerson, June 1977.
120 Some Meteorological Aspects of Air Pollution in Utah with Emphasis on the Salt Lake Valley. Dean N. Jackman and William T. Chapman, June 1977.
121 Climatological Prediction of Cumulonimbus Clouds in the Vicinity of the Yucca Flat Weather Station. R. F. Quiring, June 1977.

NOAA SCIENTIFIC AND TECHNICAL PUBLICATIONS

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